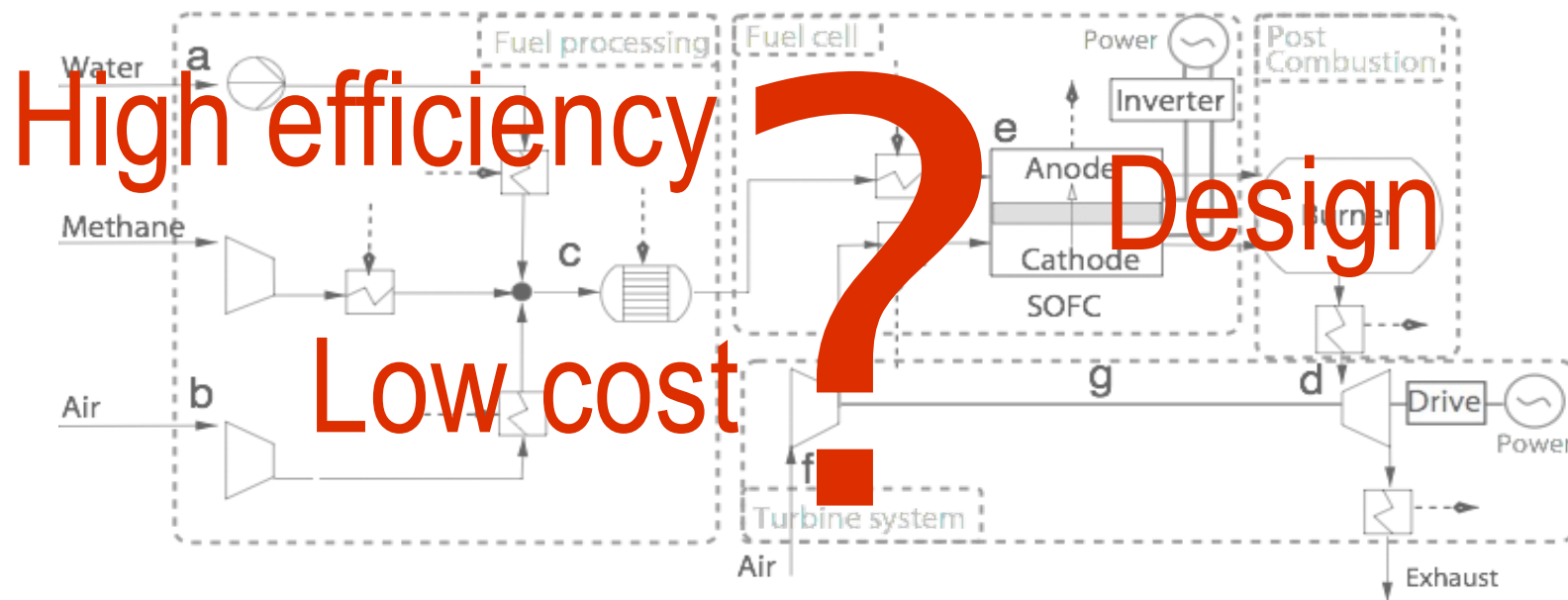


Thermo-economic Optimization of a Solid Oxide Fuel Cell, Gas Turbine Hybrid System

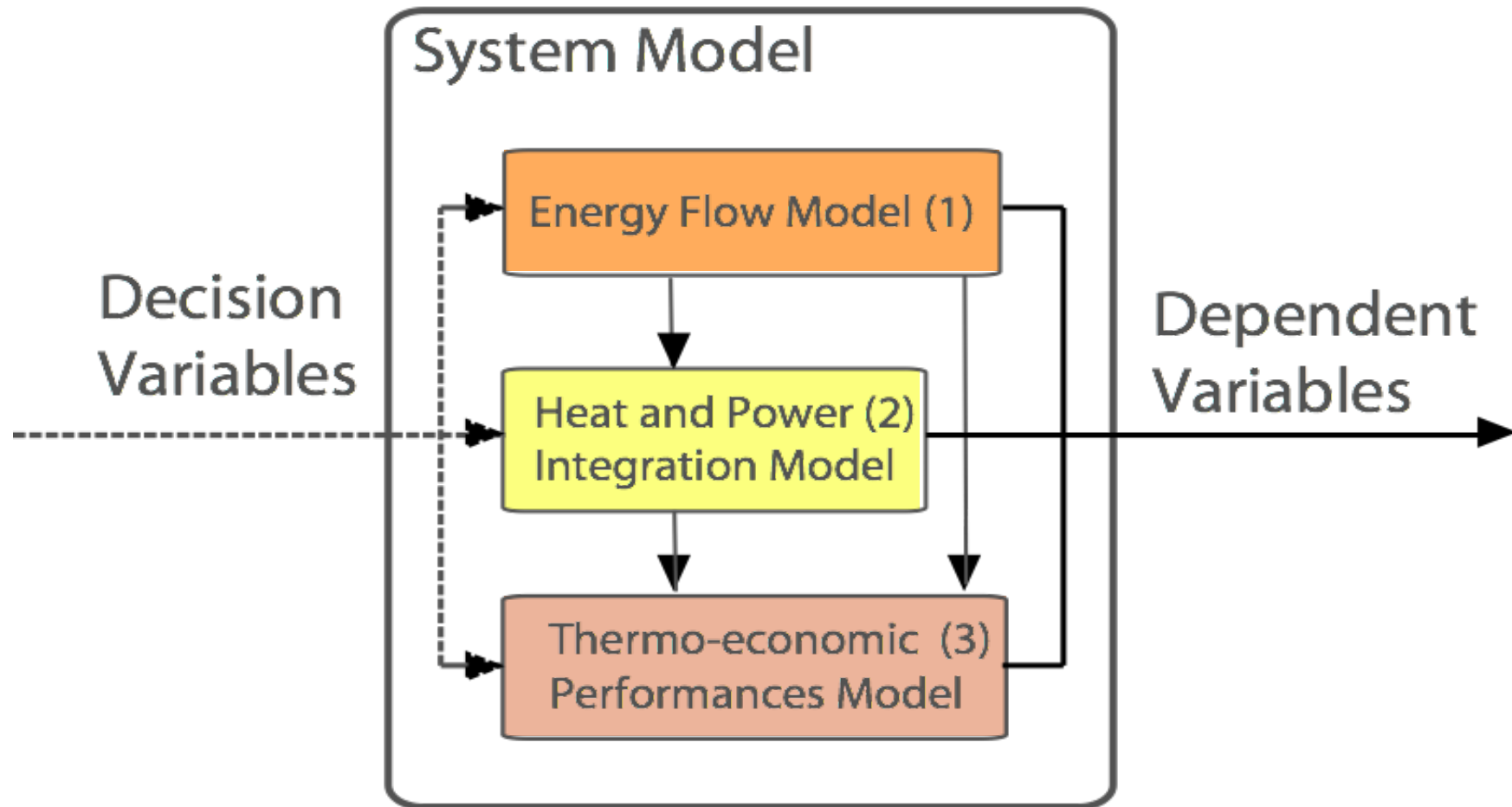


Goal and methodology

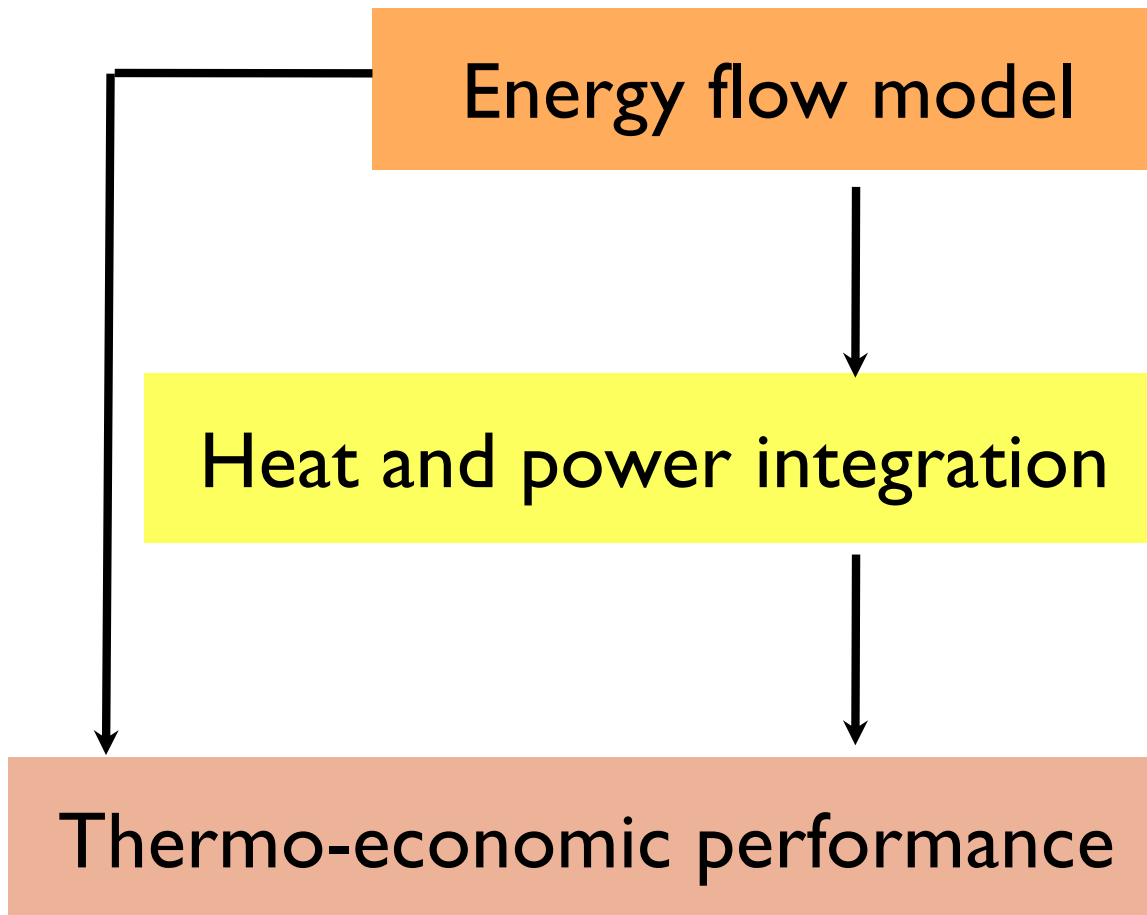
Optimal design of Fuel Cells (FC) systems where the configuration is unknown a priori



Modeling the system



Modeling tools



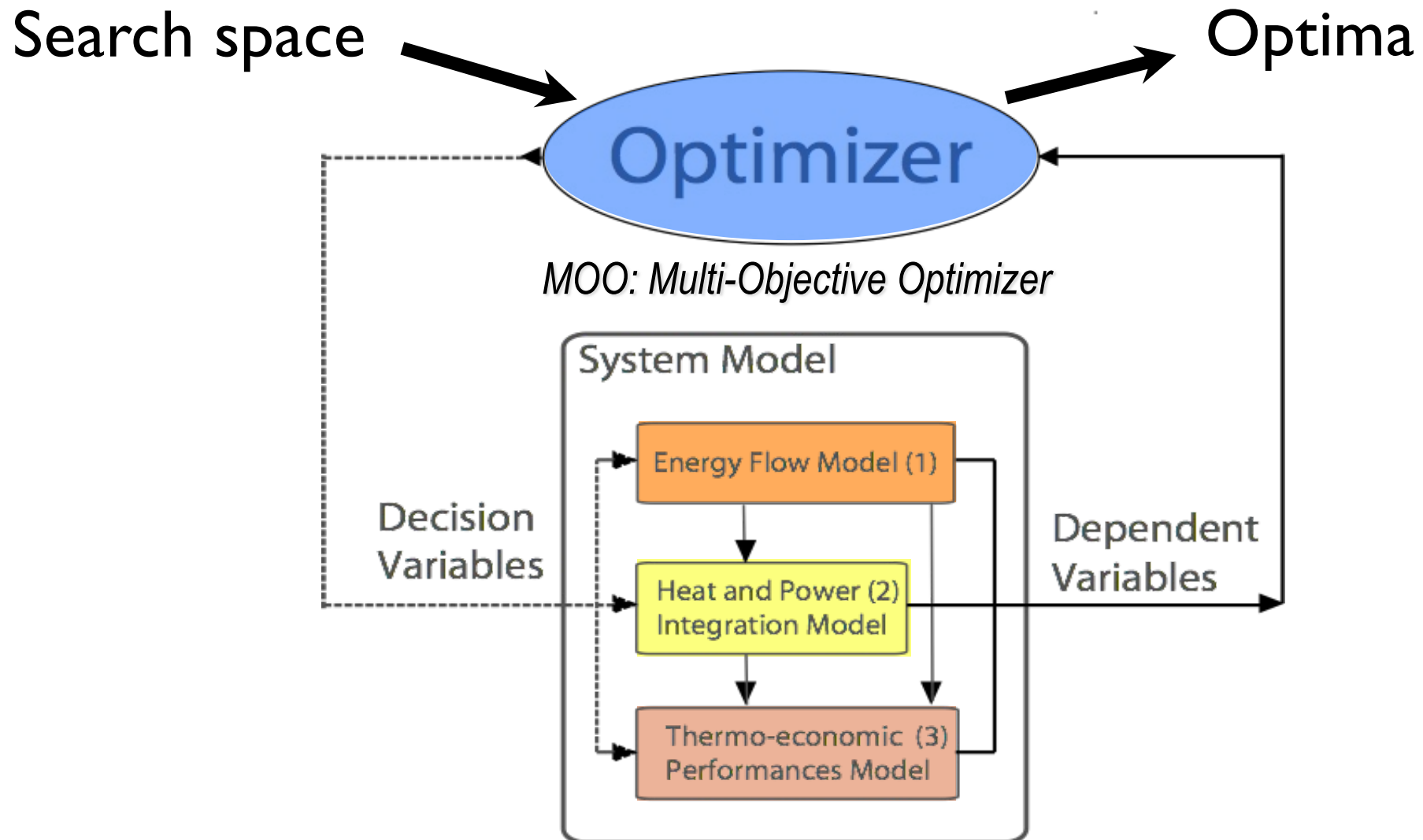
System performances

Software : Matlab

- Sequential computation
- The **sizing** of the components is computed to reach the required thermodynamic state
- The **costing** is then computed knowing the components sizes

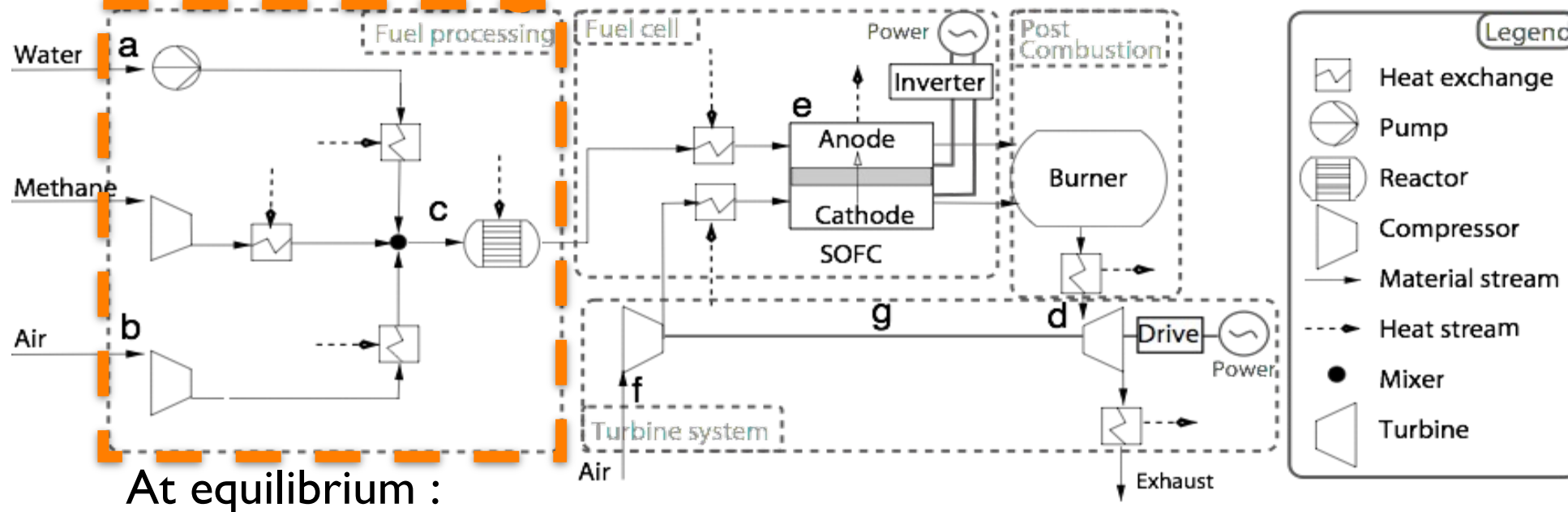
OSMOSE - under development at EPFL-IPESE

Optimize the model



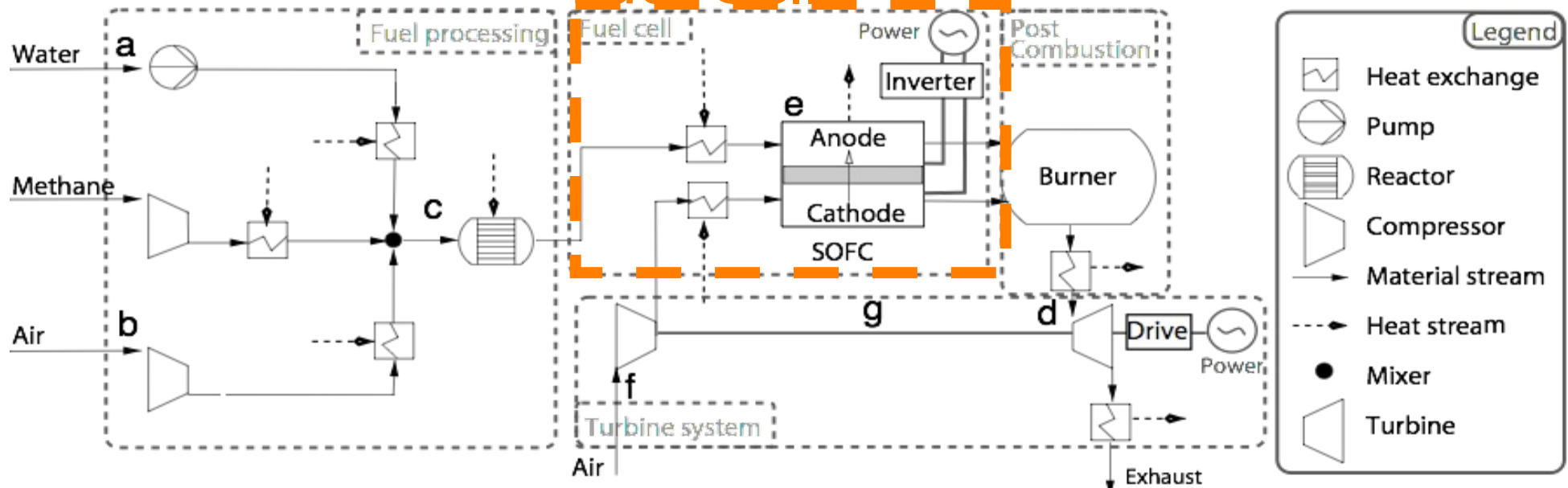
SOFC- μ GT model (30 kWe net output)

Fuel Processing



- Steam methane reforming (SMR)
- Partial oxidation (POX)
- Combination of two

Fuel Cell



- Planar anode supported cells with LSM cathode
- Operating temperature : 800°C
- 200 cm² active area
- 100 K maximum gradient in stack
- Cost calculations : cell area, number of 100 cells stacks, housing.

Fuel cell costs

$$C_{cell} = A_{cell} \cdot C_{spec}$$

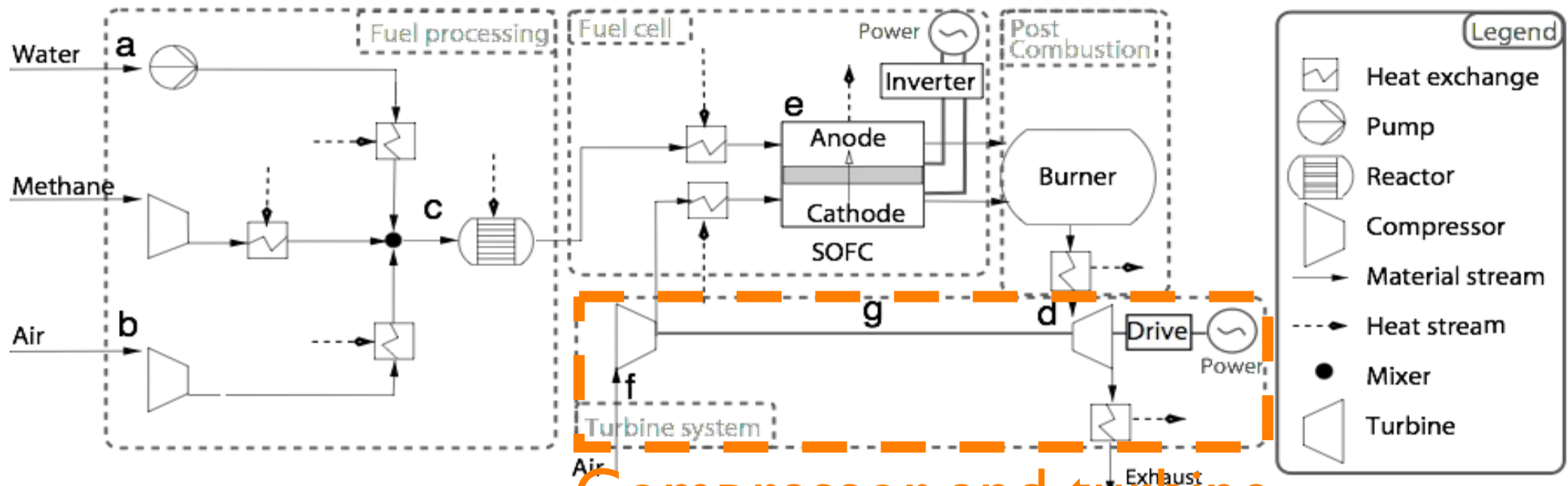
$$N_{stack} = \frac{N_{cells}}{N_{cells}^{max}}$$

$$C_{VolumeBareModule} = C_{VolumePurchase} \cdot f_{BM} \cdot f_{pressure}$$

$$C_{volumepurchase} = 10^{K_1 + K_2 \log_{10}(ThermalLoad)}$$

$$C_{FCstack} = f_{BM} \cdot (C_{cell} \cdot N_{cells} + 2 \cdot N_{stack} \cdot A_{cell} \cdot f_{hs} \cdot C_{h,spec})$$

$$C_{fc} = f_{actualization} \cdot (C_{VolumeBareModule} + C_{FCstack})$$



Compressor and turbine

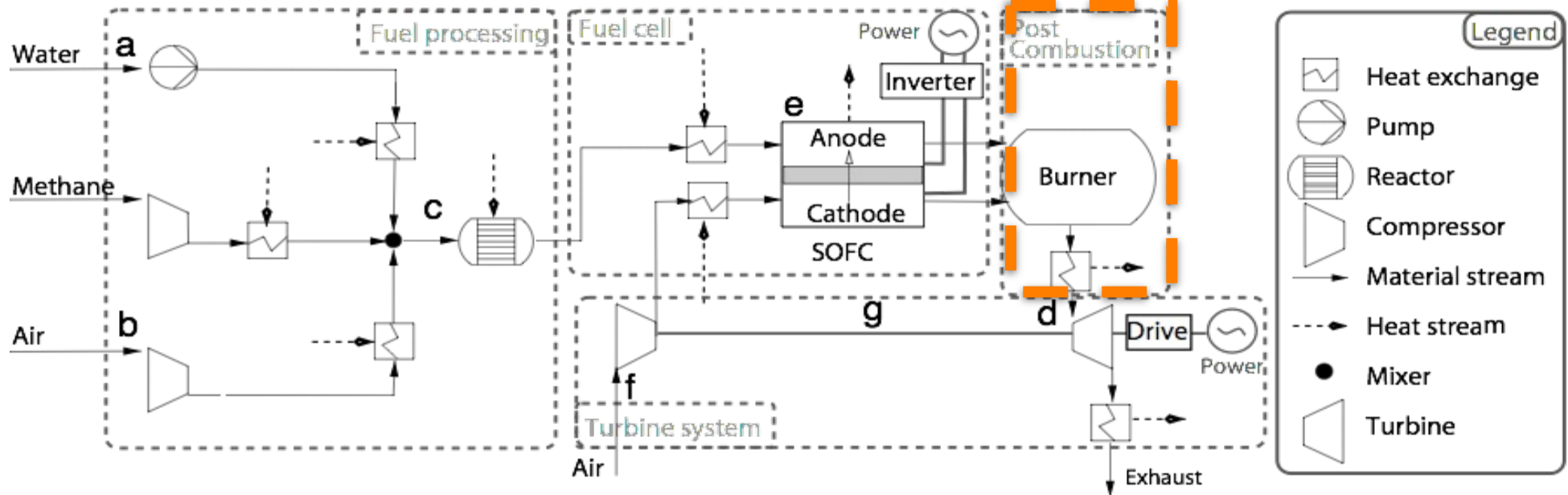
- High speed compressor and turbine (> 100 000 rpm)
- Single shaft
- Air bearings technology
- Rotational speed, diameter, tip speed and efficiencies are computed

Gas Turbine costs

$$C_{Drive} = P_{shaft} \cdot C_{DriveSpec}$$

$$C_{microGT} = f_{actualization} \cdot (C_{Drive} + C_{ct})$$

Post-combustion



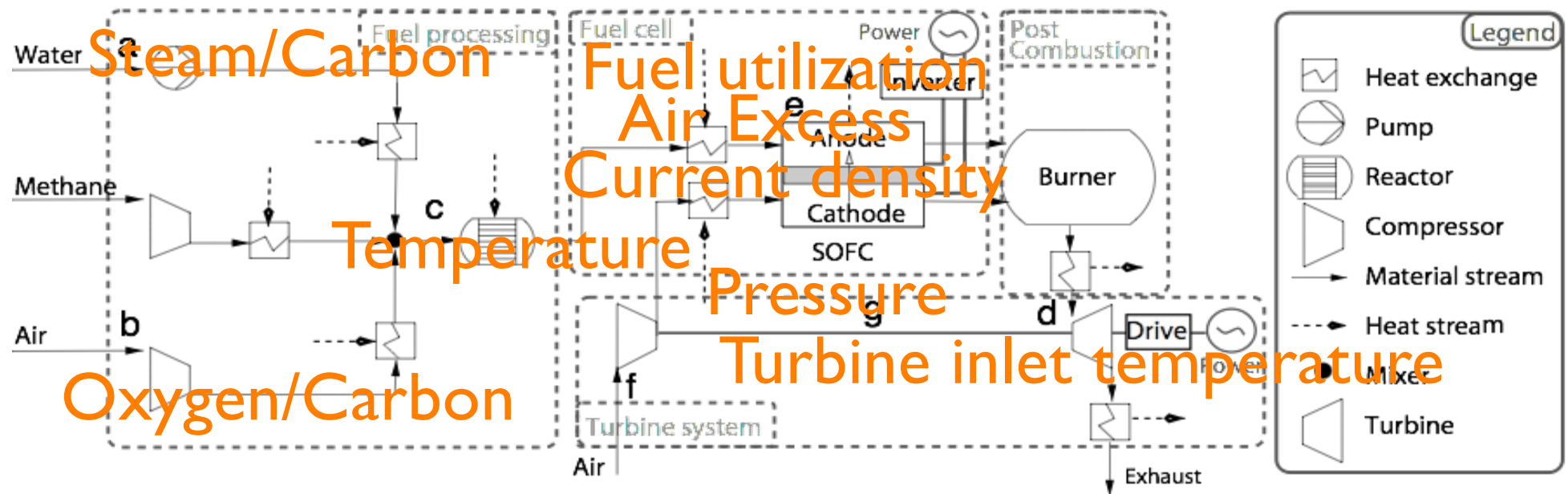
- Complete combustion of anode depleted gas
- Heat exchanger to lower temperature to turbine inlet temperature

Optimization

Two objectives:

- Maximum **Efficiency**
- Minimum **installed Cost**

Search space



30 kWe hybrid cycle

pressurized SOFC with high speed μ GT

Search space

Fuel utilization	[0.5 ; 0.80]	-
Pressure	[1.1 ; 6]	bar
Oxygen to carbon ratio	[0.001 ; 0.5]	-
Steam to carbon ratio	[0.4 ; 4]	-
Turbine inlet temperature	[800 ; 1350]	K
Air excess ratio	[1.5 ; 5]	-
Current density	[1000 ; 5000]	A/m ²
Reformer temperature	[800 ; 1100]	K

Fuel cell equations (1)

Non-ohmic losses

Cathode

Butler Volmer current overpotential $i = i_{0,c} \cdot \left(e^{\frac{F}{2RT_s} \cdot \eta_c} - e^{-\frac{F}{2RT_s} \cdot \eta_c} \right)$

Cathode base current $i_{0,c} = \frac{2 \cdot R \cdot T_s \cdot \sigma_c}{F}$

Cathode conductance $\sigma_c = \sigma_{0,c} \cdot e^{-\frac{E_{A,c}}{R \cdot T_s}}$

Anode

Butler Volmer current overpotential $i = i_{0,a} \cdot \left(e^{\frac{2F}{RT_s} \cdot \eta_a} - e^{-\frac{F}{RT_s} \cdot \eta_a} \right)$

Anode base current $I_{0,a} = \frac{R \cdot T_s \cdot \sigma_a}{3F}$

Anode conductance $\sigma_a = \sigma_{0,a} \cdot e^{-\frac{E_{A,a}}{R \cdot T_s}}$

Fuel cell equations (2)

Electro-chemical

Current $I = \frac{\dot{n}_{O_2,m} \cdot 4F}{N_{cells}}$

Power $\dot{E}_{FC}^- = -\Delta G_{stack} - R_{tot} \cdot I^2 - (\eta_a + \eta_c + \eta_{diff,a} + \eta_{diff,c}) \cdot N_{cells} \cdot I$

Available gibbs free enthalpy flow $\Delta \dot{G}_{stack} = (\dot{G}_{c,out} + \dot{G}_{a,out}) - (\dot{G}_{c,in} + \dot{G}_{a,in})$

Current density $i = \frac{I}{A_{cell}}$

Stack potential $U = \frac{\dot{E}_{FC}^-}{I}$

Cell potential $U_{cell} = \frac{U}{N_{cells}}$

Fuel cell equations (3)

other model equations

Fuel utilization $\mu = \frac{\dot{n}_{O_2,m}}{\dot{n}_{O_2,c,in} - \dot{n}_{O_2,pc,out}}$

Air excess $\lambda = \frac{\dot{n}_{O_2,c,in} + \dot{n}_{O_2,fp,in}}{\dot{n}_{O_2,c,in} + \dot{n}_{O_2,fp,in} - \dot{n}_{O_2,pc,out}}$

Ohmic losses

Total resistive loss $R_{tot} = R_i + R_e$

Interconnect resistive loss $R_i = \frac{R_{i,a} + R_{i,c}}{A_{cell}} \cdot N_{cells}$

Electrolyte resistive loss $R_e = \frac{1}{\sigma_e} \cdot \frac{L_e}{A_{cell}} \cdot N_{cells} \cdot f_{cc}$

Electrolyte conductance $\sigma_e = \sigma_{0,e} \cdot e^{-\frac{E_{A,e}}{RT_s}}$

Diffusion losses

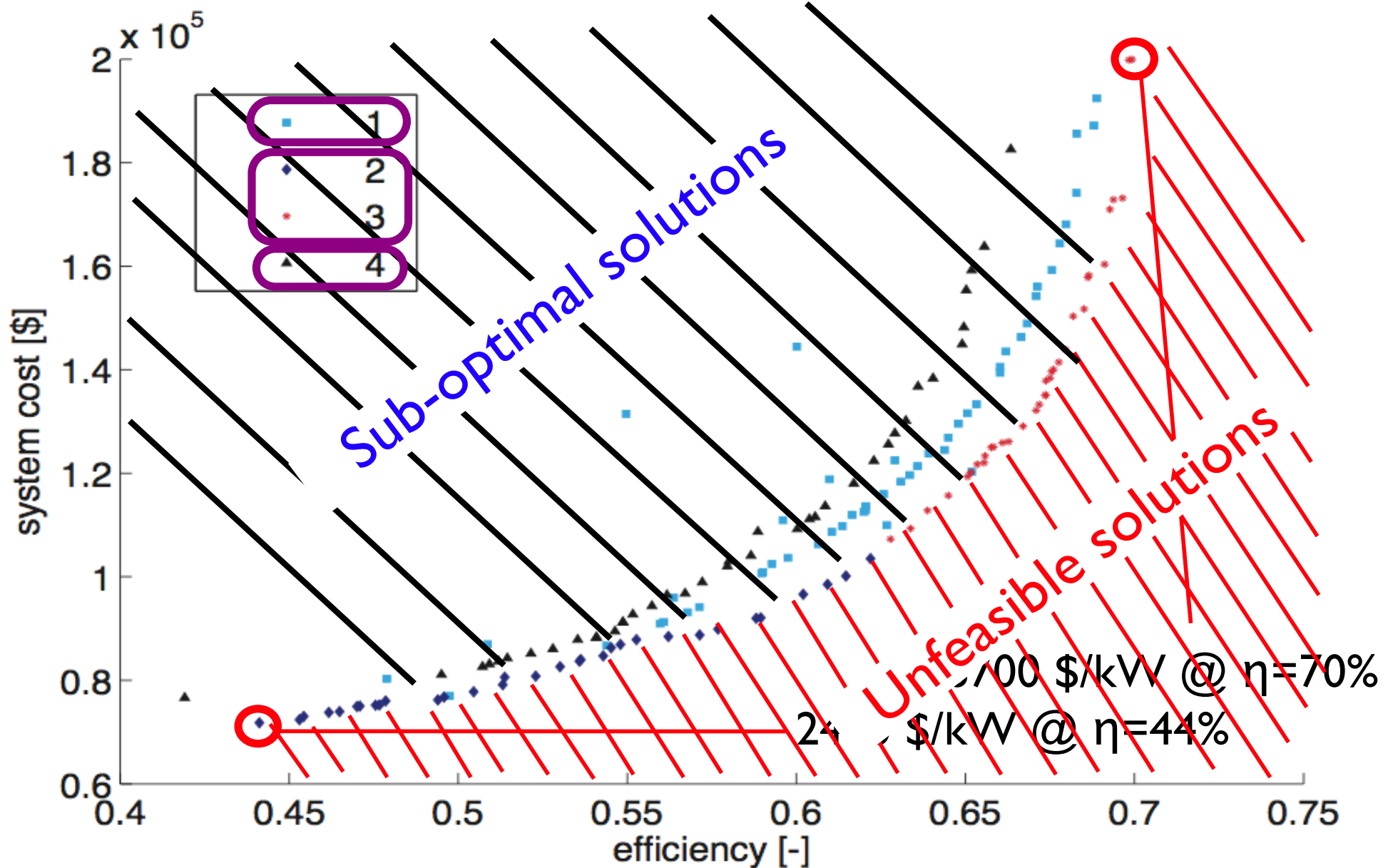
Anode polarization $\eta_{diff,a} = -\frac{RT_a}{2F} \cdot \log(1 - \mu)$

Cathode polarization $\eta_{diff,c} = -\frac{RT_s}{2F} \cdot \log(1 - \frac{\mu}{\lambda})$

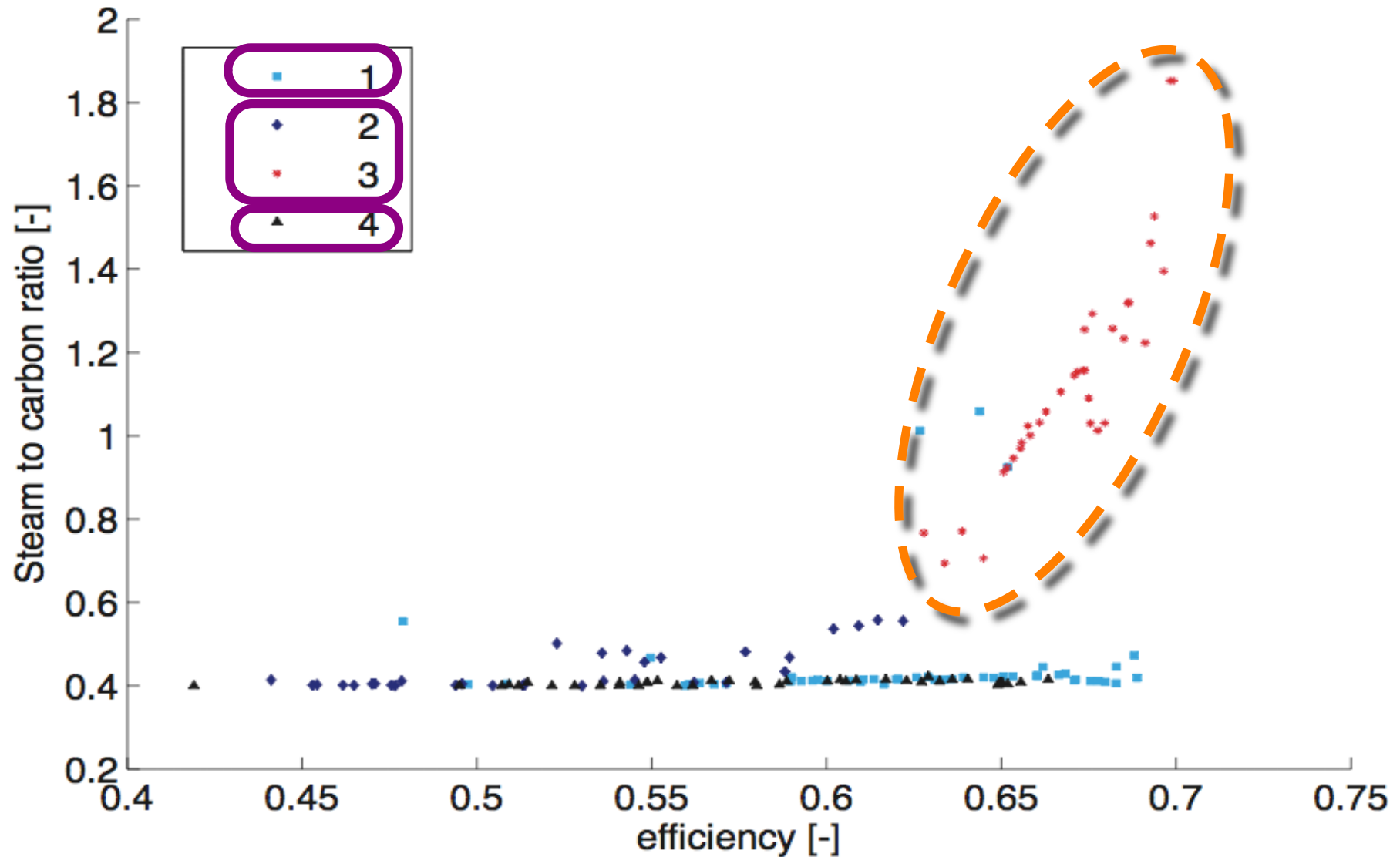
Chemical reaction equations

Name	Reaction	Reaction enthalpy
Steam methane reforming	$CH_4 + H_2O \leftrightarrow CO + 3H_2$	$\Delta H_0 = 206.11 kJ/mol$
Water gas shift	$CO + H_2O \leftrightarrow CO_2 + H_2$	$\Delta H_0 = -41.160 kJ/mol$
Hydrogen combustion	$2H_2 + O_2 \rightarrow 2CO_2$	$\Delta H_0 = -571.6 kJ/mol$
carbon monoxide combustion	$2CO + O_2 \rightarrow 2CO_2$	$\Delta H_0 = -565.8 kJ/mol$
Methane partial oxydation	$CH_4 + \frac{1}{2}O_2 \rightarrow CO + 2H_2$	$\Delta H_0 = -35.715 kJ/mol$

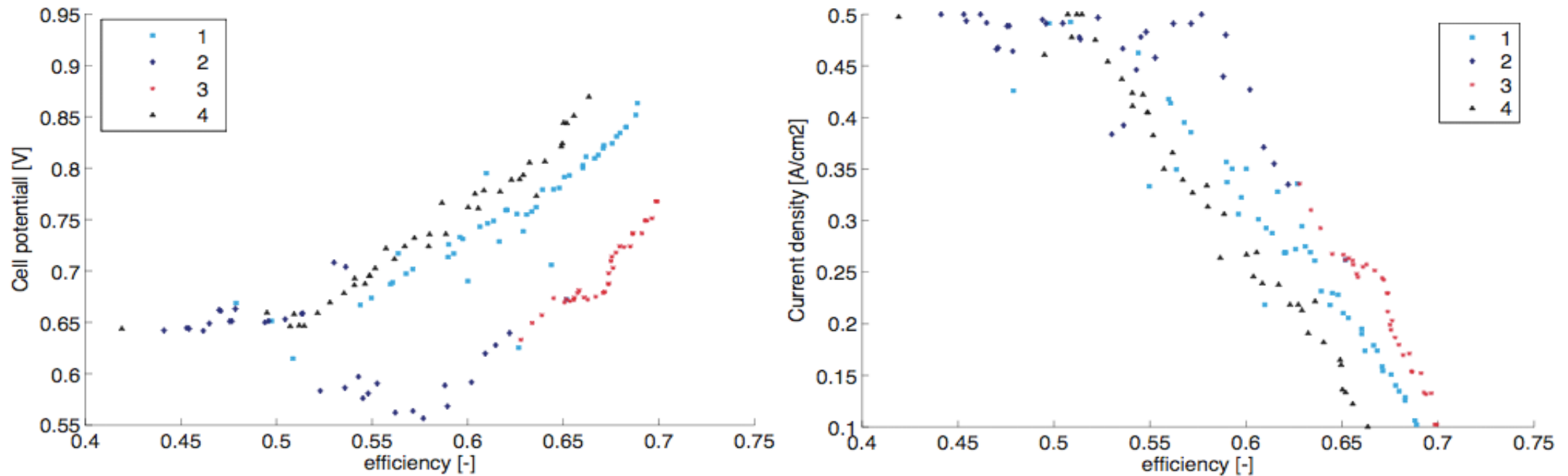
Tradeoff: Efficiency - System Cost



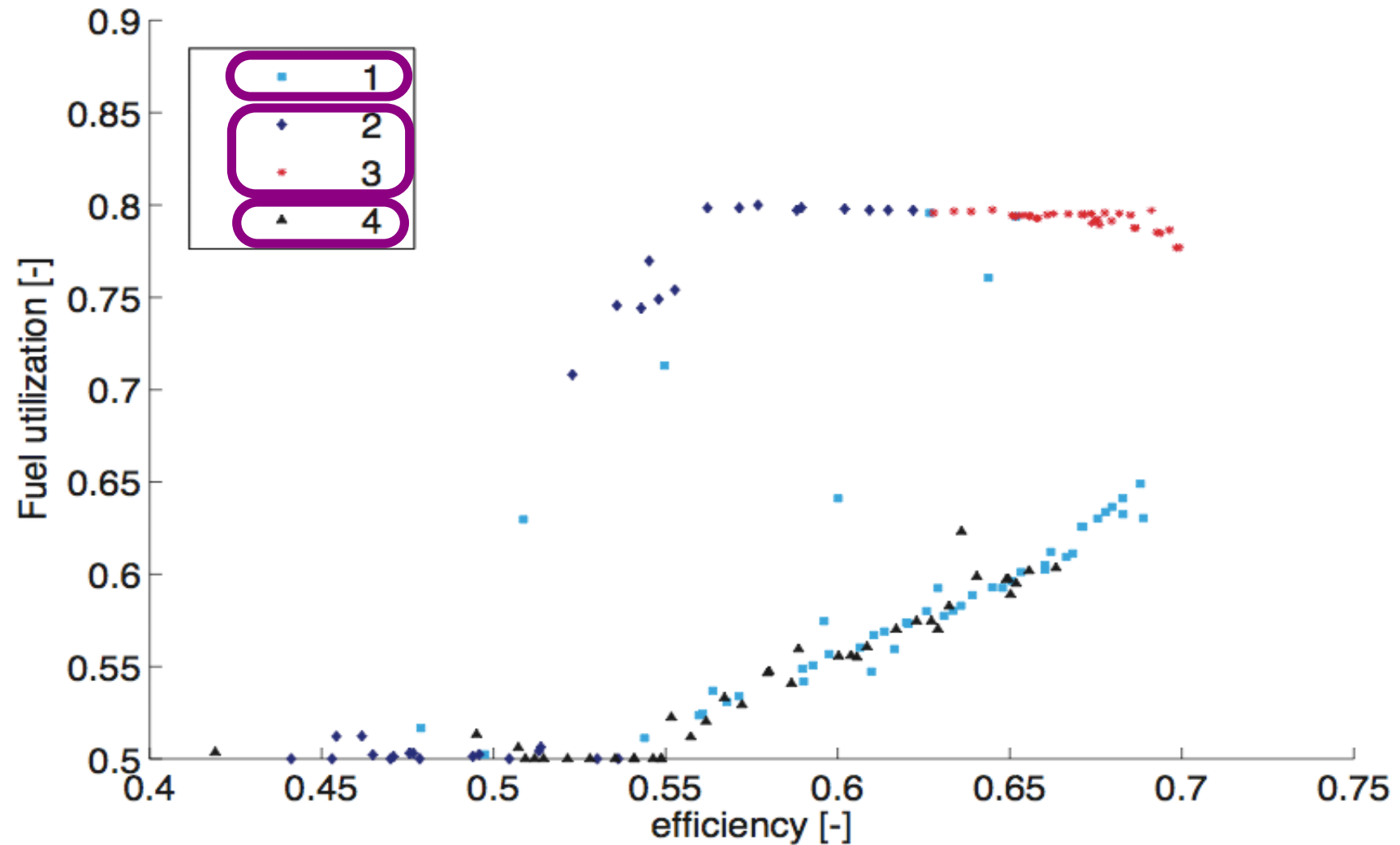
Steam to Carbon ratio



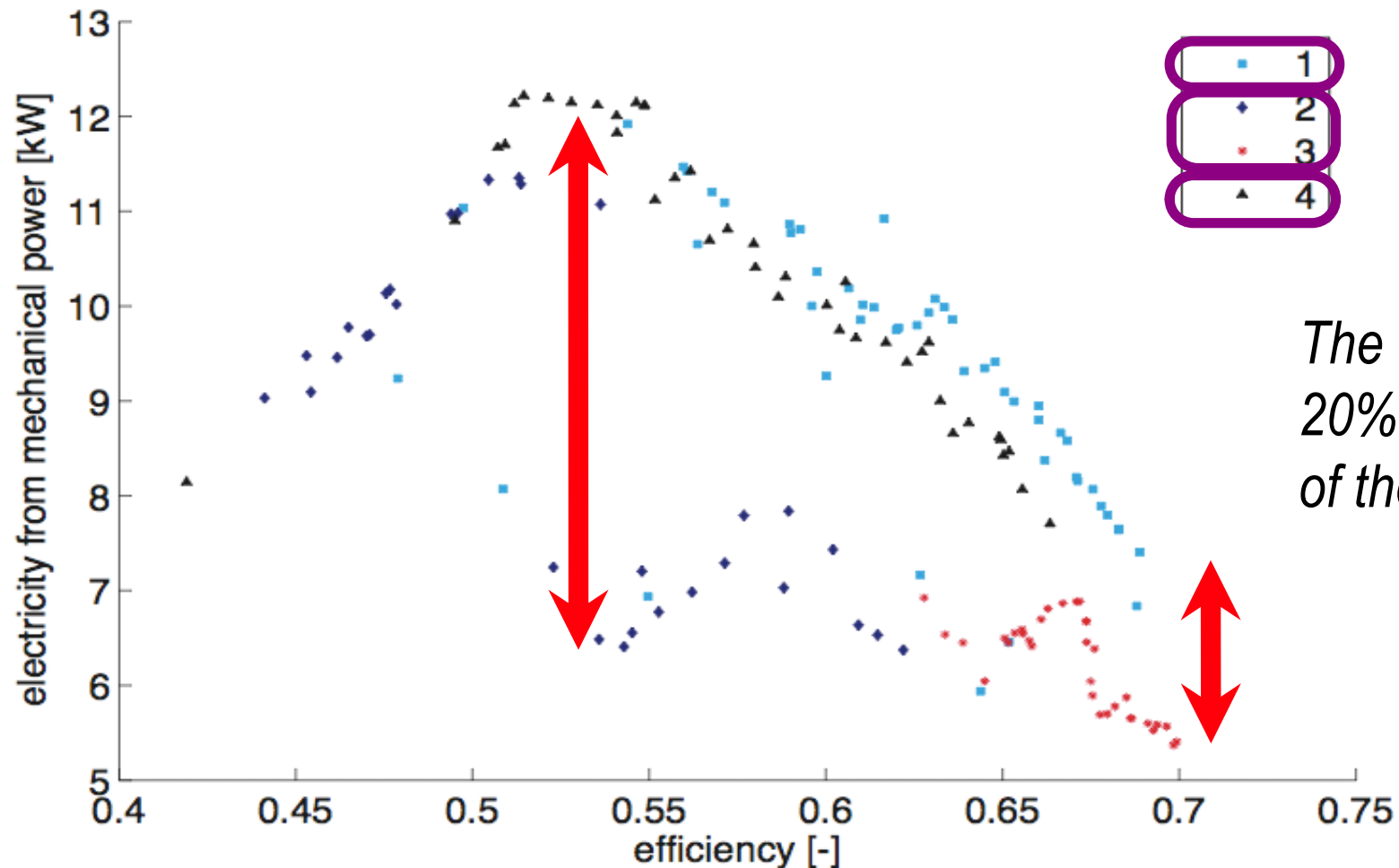
Cell potential & current density



Fuel utilization

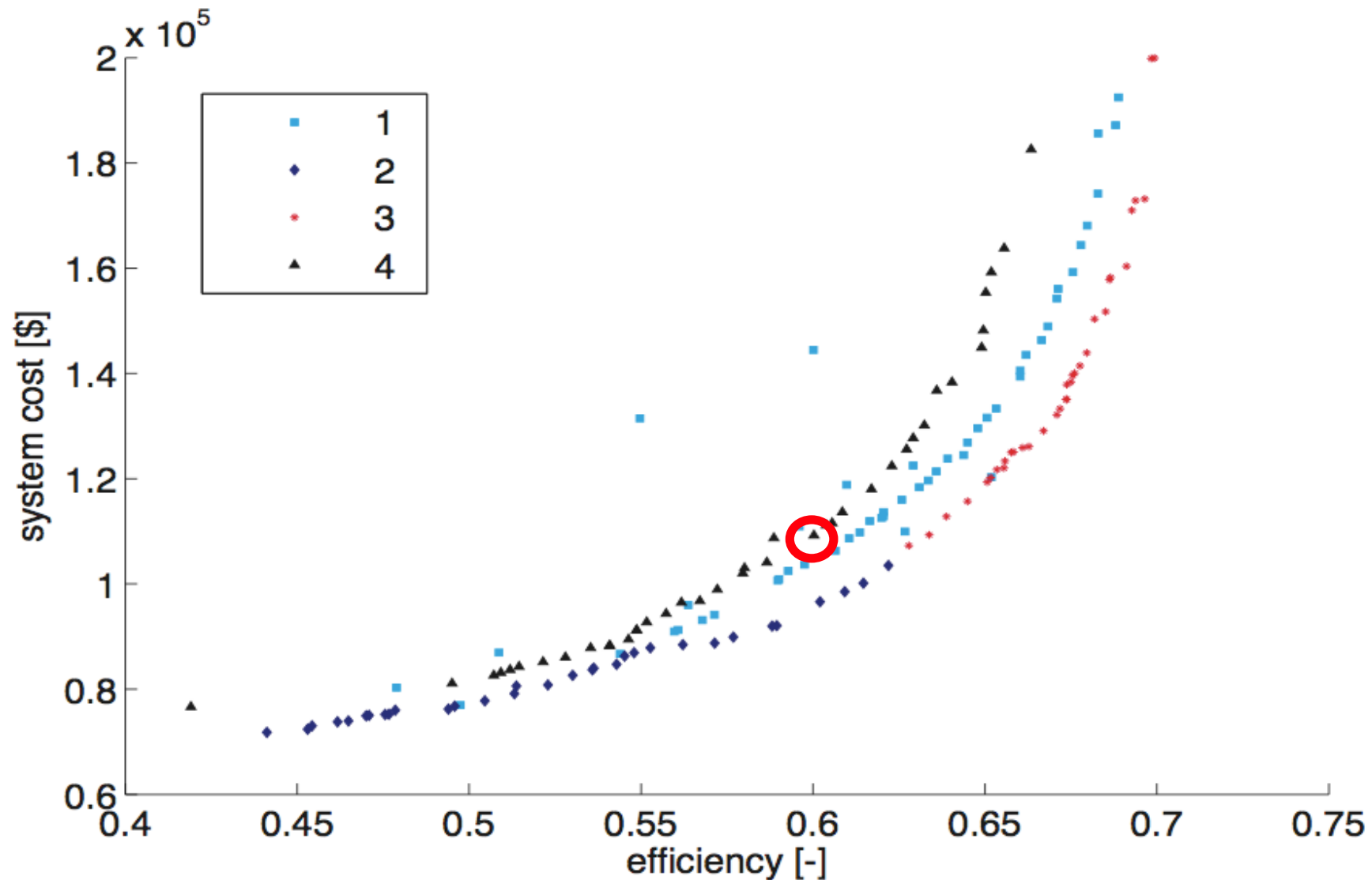


Turbine power

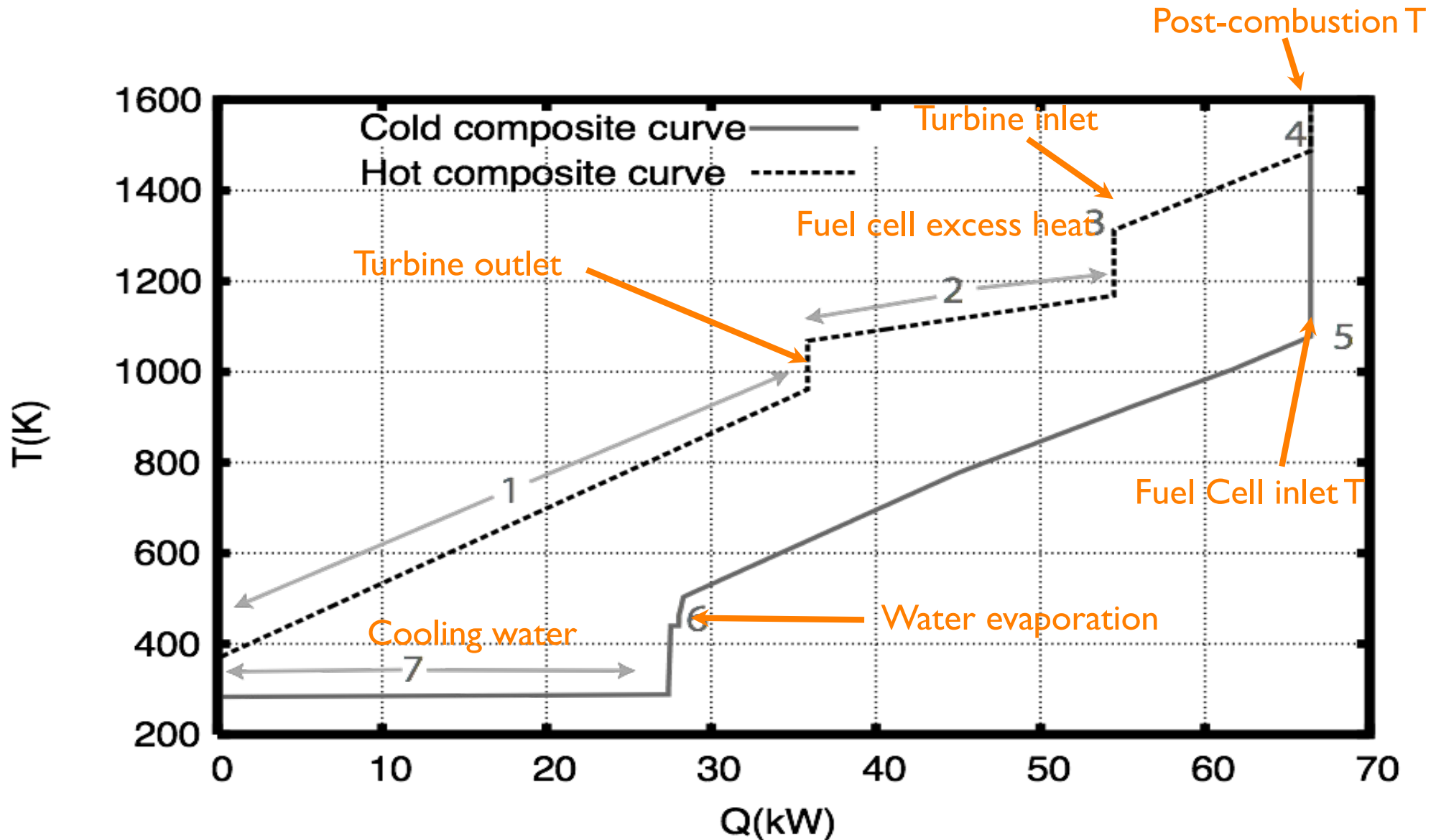


*The turbine delivers
20% to 40%
of the total power*

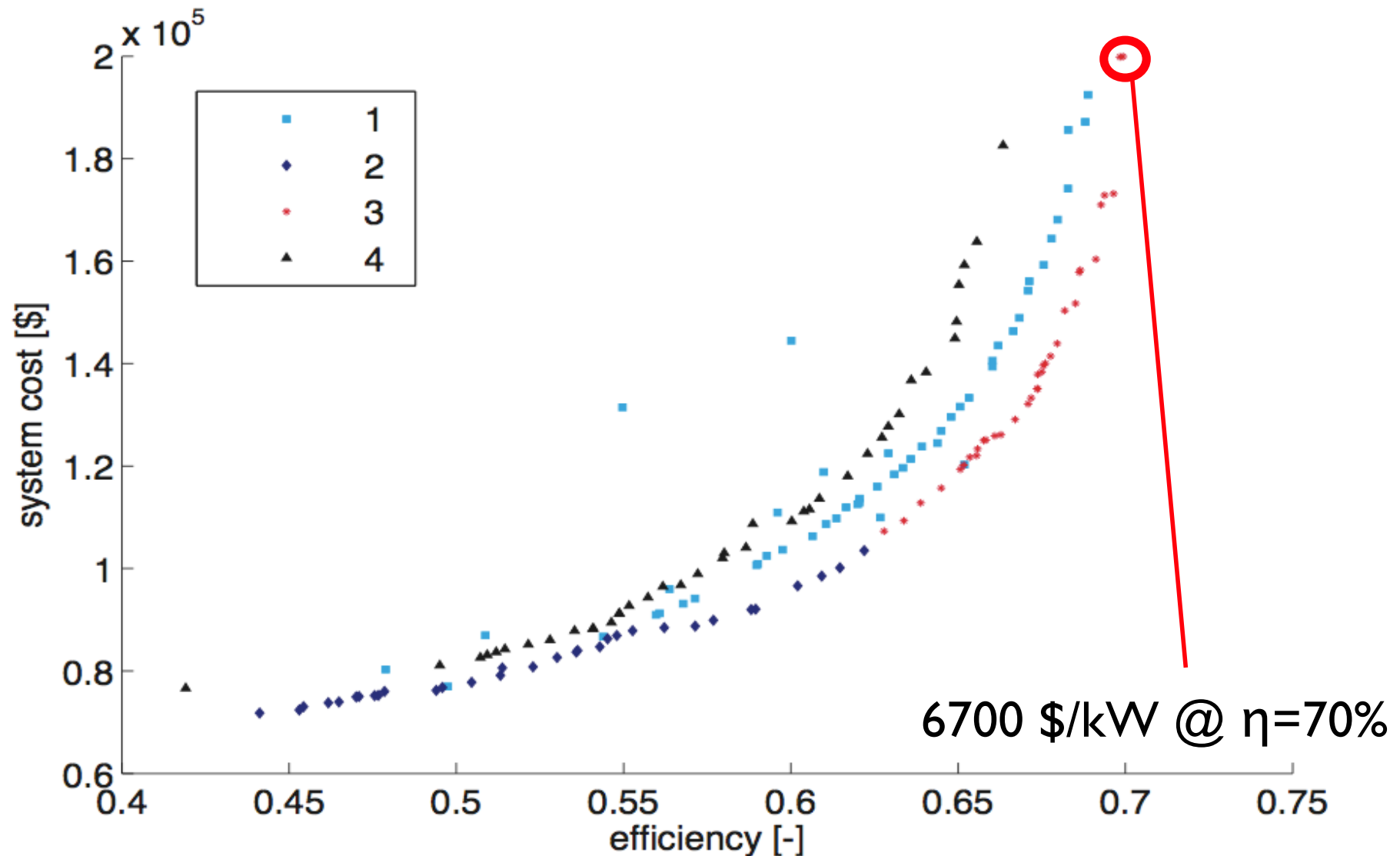
Heat integration example



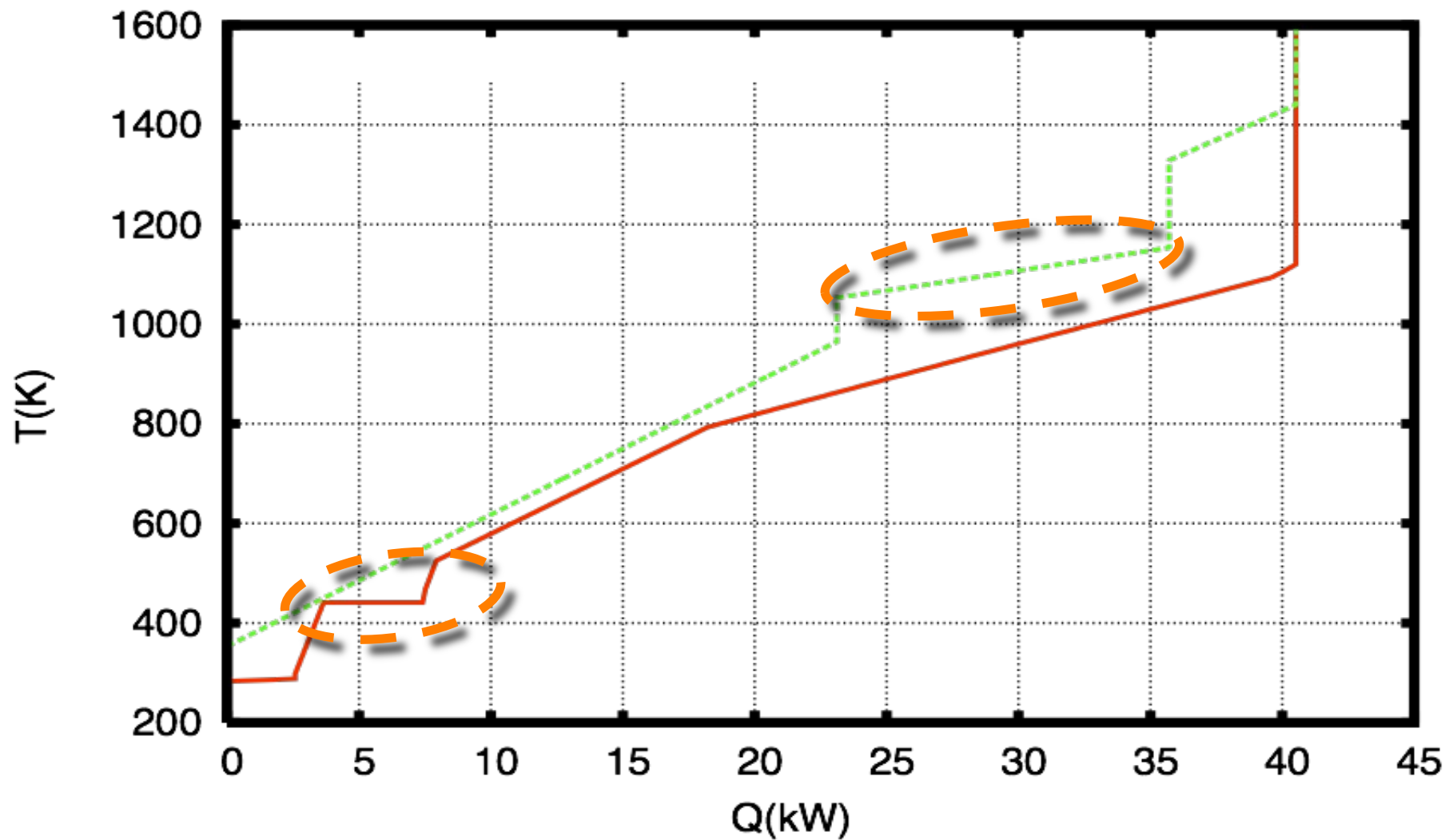
Heat integration example



Most efficient case:

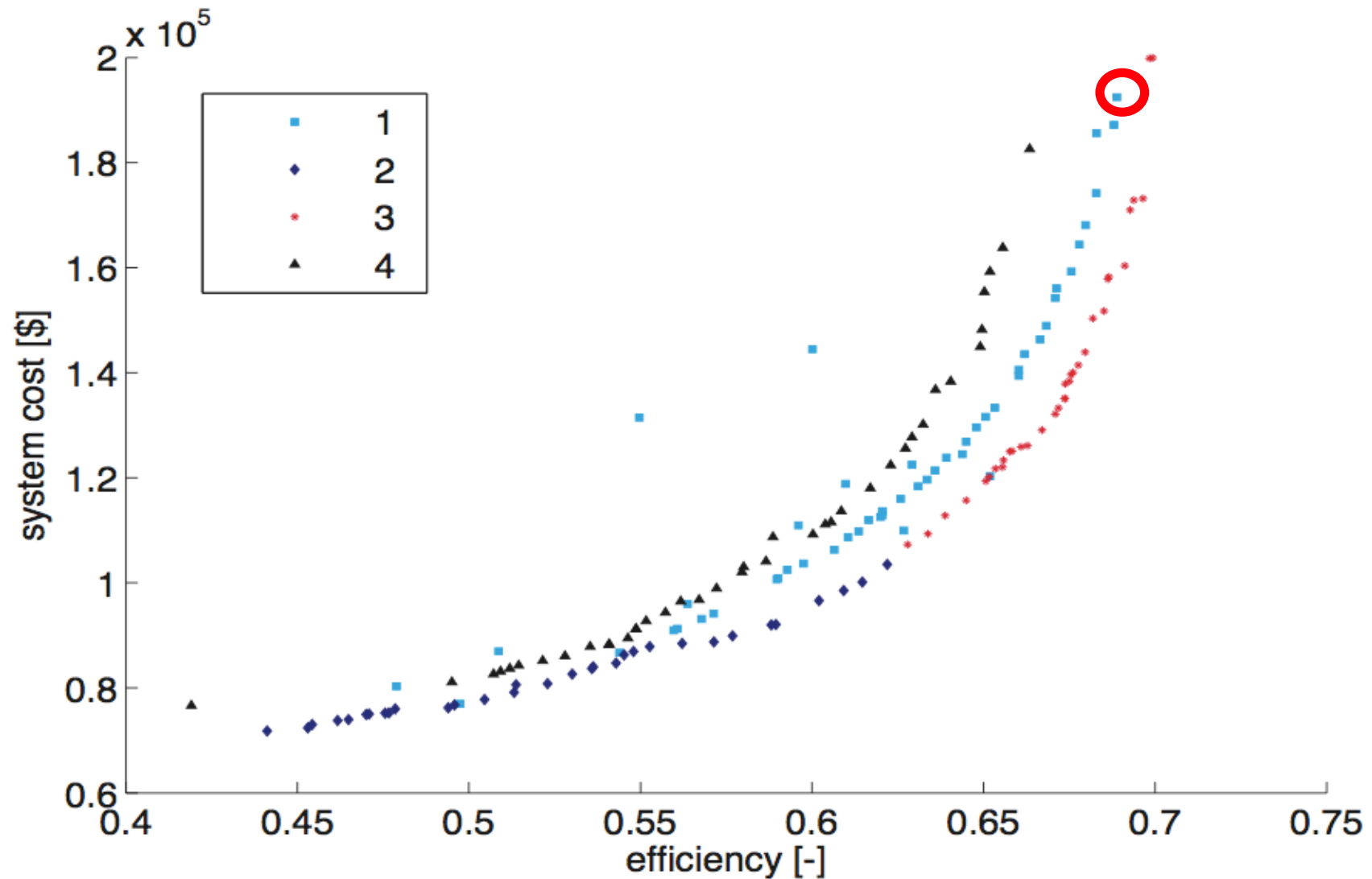


Most efficient case:

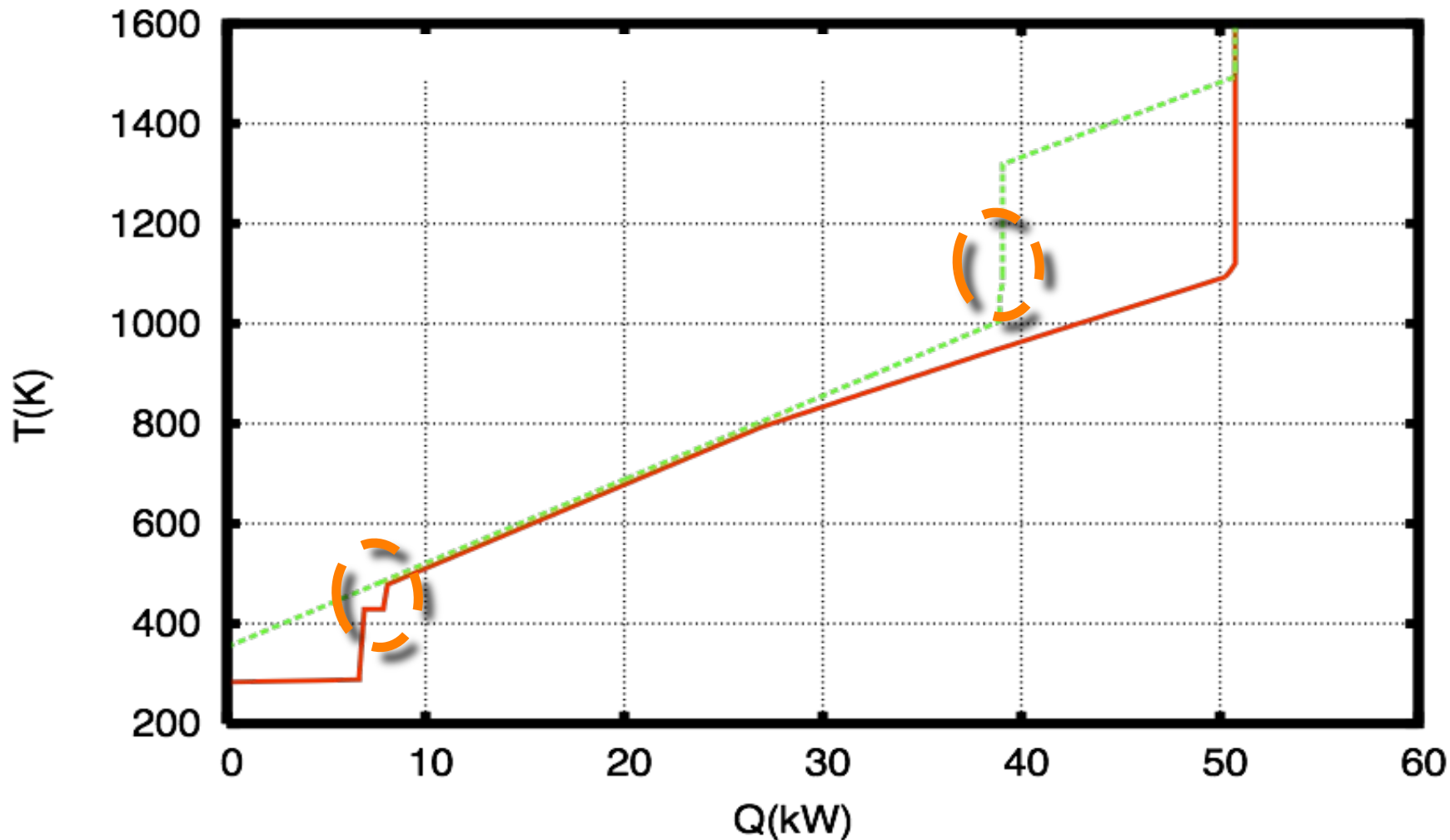


$$\begin{aligned} S/C &= 2 \\ \eta &= 0.70 \\ \lambda &= 1.9 \end{aligned}$$

Another high efficiency case...



...shows a very distinct configuration

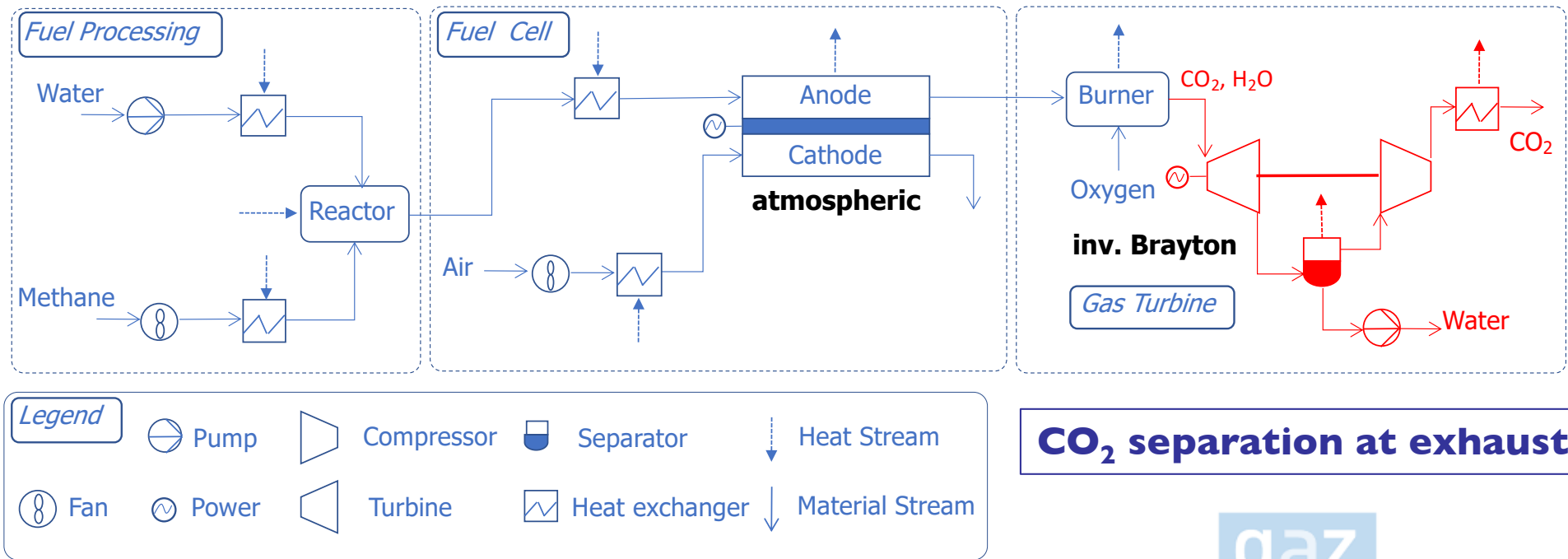


$$\begin{aligned} S/C &= 0.4 \\ \eta &= 0.69 \\ \lambda &= 3.2 \end{aligned}$$

SOFC + microgasturbine



Prof Jürg Schiffmann



CO₂ separation at exhaust



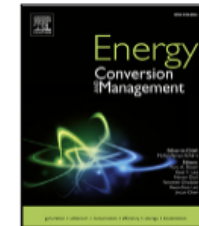
State of the Art Analysis



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Review

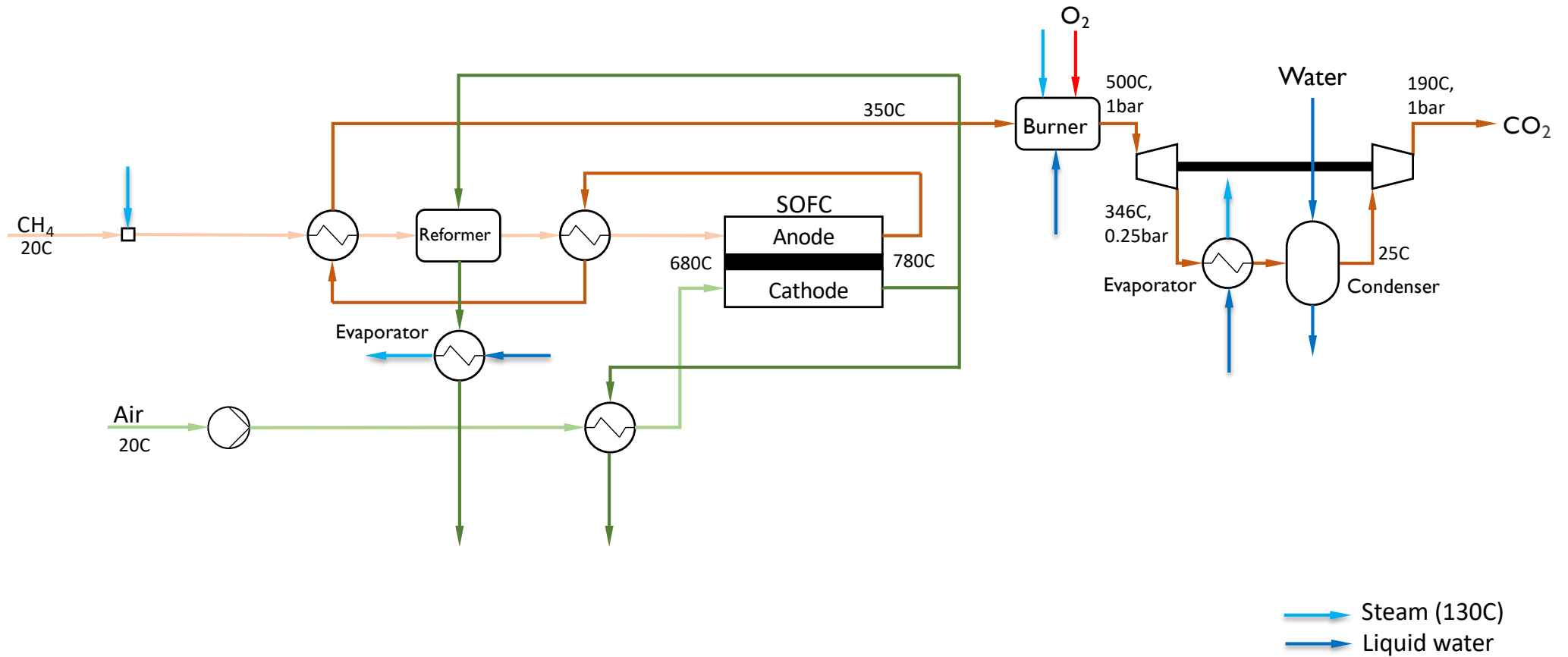
Readiness evaluation of SOFC-MGT hybrid systems with carbon capture for distributed combined heat and power

Victoria He^a, Michele Gaffuri^{a,*}, Jan Van herle^b, Jürg Schiffmann^a

[Volume 278](#), 15 February 2023, 116728



Selected Heat Exchanger Network



Micro Gas Turbine

- Inverted Brayton-Ranking Cycle
 - Subatmospheric Expansion
- Micro Gas Turbine:
 - 1.5 kWe
 - > 300'000 RPM
 - Gas Bearing Supported
 - Integrated Electrical Machine
- Research challenges
 - Extreme Temperature
 - High Thermal Gradient
 - Bearings μm Clearances
 - Integrated Multiphysics Optimization

